The Trident® Acetabular System has been implanted throughout the world since 1999 and, while commercially available, has also been included in a clinical evaluation through an IDE study in the United States. All Trident® Acetabular Shells feature the Innerchange™ Locking Mechanism, which provides independent locking of polyethylene or ceramic inserts into the shell.

**The Trident® Acetabular System offers:**
- Superior locking mechanisms for both polyethylene and ceramic inserts
- X3™ polyethylene for improved wear performance
- Choice of shell geometries
- Arc-deposited roughened surface to help achieve immediate stability
- Purefix™ HA
- Eccentric and Constrained Inserts for revision options

**Trident® PSL® HA Acetabular Shell**

The Trident® PSL® Acetabular Shells are designed to maximize fixation in the peripheral lunate region of the acetabulum. Purefix™ HA coating is featured on all Trident® PSL® shells.

**Trident® Hemispherical Acetabular Shell**

Trident® Hemispherical Acetabular Shells are a true hemispherical shape designed to achieve press-fit fixation by underreaming the acetabulum.
The Patented Innerchange™ Locking Mechanism allows for independent locking of polyethylene and ceramic inserts into the shell. This provides radial and tilting micromotion resistance.

The Trident® polyethylene insert allows for proper rotational alignment using 12 indexable scallops. Polyethylene inserts lock into the shell in three ways:

- Four alignment studs on the shell provide proper rotational and axial alignment
- Unique bead and groove mechanism
- Additional rim locking provides for exceptional insert stability

According to Dr. Litsky's study, among the designs from other manufacturers, none is better than the Stryker® Trident® design in either radial or tilting micromotion.¹

Extensively Tested Locking Mechanism
- Fully congruent design
- Independent testing by Alan Litsky, MD, PhD at Ohio State University ¹
- Robust push-out and lever-out resistance²
- Hip simulation testing with X3™ polyethylene has demonstrated improved wear performance³,

Micromotion (µm)

<table>
<thead>
<tr>
<th>Manufacturer</th>
<th>Radial</th>
<th>Tilting</th>
</tr>
</thead>
<tbody>
<tr>
<td>Stryker® Trident®</td>
<td>4</td>
<td>5</td>
</tr>
<tr>
<td>Biomet Ringloc</td>
<td>6</td>
<td>4</td>
</tr>
<tr>
<td>Biomet Reflection</td>
<td>8</td>
<td>6</td>
</tr>
<tr>
<td>J&amp;J PFC®</td>
<td>6</td>
<td>8</td>
</tr>
<tr>
<td>Zimmer Trilogy™</td>
<td>9</td>
<td>12</td>
</tr>
<tr>
<td>DePuy Duraloc™</td>
<td>7</td>
<td>19</td>
</tr>
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</table>

¹ According to Dr. Litsky's study, among the designs from other manufacturers, none is better than the Stryker® Trident® design in either radial or tilting micromotion.

² Independent testing by Alan Litsky, MD, PhD at Ohio State University.

³ Hip simulation testing with X3™ polyethylene has demonstrated improved wear performance.
Polyethylene
Trident® polyethylene inserts are:
• Fully congruent to the shell
• Supported by extensive research on range of motion and head stability
• Available in neutral, 10˚, elevated rim, eccentric and constrained designs

Neutral, 10˚ and Elevated Rim polyethylene options
X3™ Highly Crosslinked Polyethylene

X3™ Highly Crosslinked polyethylene has demonstrated significant wear reduction compared to standard polyethylene. Stryker’s technology and conservative process have allowed increased crosslinking while maintaining the material properties of the polyethylene.

- **97% reduction in wear**
  X3™ polyethylene demonstrates 97% reduction in wear over nitrogen sterilized polyethylene in joint simulation testing, thereby reducing the potential for osteolysis.

- **Material properties are retained**
  The material properties of X3™ polyethylene are similar to those of standard polyethylene, as shown in Figure 1.

- **Preserves the polymer structure of UHMWPE**
  The crystalline and amorphous regions of X3™ are similar to standard polyethylene (Figure 2).

Figure 1 X3™ polyethylene maintains similar yield strength, modulus and crystallinity as standard polyethylene. When these properties change significantly, the clinical wear performance cannot be predicted.

Figure 2 X3™ exhibits a morphology that is very similar to that of standard UHMWPE.
**LFIT™ Technology**

**Improved Wear Performance with LFIT™ Femoral Head Technology**

Low Friction Ion Treatment (LFIT™) is a bombardment of nitrogen ions onto a CoCr surface, which enhances material properties of the metal, in turn reducing frictional forces against UHMWPE surfaces.

**LFIT™:**
- Improves wettability
- Reduces coefficient of friction

**Wettable materials are important in total hip arthroplasty**

In an anatomic hip joint, the femoral head is cushioned by cartilage, which seeps lubrication into the joint. When the joint is diseased or removed, the natural lubrication surface is also removed, and the femoral head and acetabular insert contact each other. LFIT™ femoral heads are designed to increase lubrication.

**Clinical Experience with LFIT™**

The LFIT™ heads demonstrated a 28% reduction in linear wear over CoCr heads in 110 patients at minimum 3-year follow up⁶ (Figure 3). This data coincides with hip simulation testing.⁶

“...These results are encouraging...Nitrogen ion implanted femoral heads may be an effective way to decrease UHMWPE wear and increase implant longevity in THA.”

**UHMWPE Linear Wear**

<table>
<thead>
<tr>
<th>Material</th>
<th>Linear Wear Rate</th>
</tr>
</thead>
<tbody>
<tr>
<td>Non-LFIT™</td>
<td>161 μm/year</td>
</tr>
<tr>
<td>CoCr LFIT™</td>
<td>116 μm/year</td>
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</table>

*Figure 3* LFIT™ heads demonstrated a 28% reduction in linear wear over CoCr heads.
Revision Options

- A Trident® Hemispherical Multi-Hole Acetabular Shell with Purefix™ HA is available providing increased screw hole options (Figure 4).
- Eccentric and Constrained Inserts augment the Trident® System with revision options to increase surgeon flexibility in complex primary or revision surgery.
- The Trident® Eccentric Inserts feature X3™ Highly Crosslinked Polyethylene for improved wear performance. The head center is lateraled 6mm from the center of the acetabular shell allowing increased polyethylene thickness and joint stability (Figure 5).
- Trident® Constrained Inserts are available for total hip patients who exhibit a risk of hip dislocation. Constrained Inserts feature pre-assembled inserts with the unique Stryker® design UHR® bipolar (Figure 6).
Compatibility

Trident® polyethylene inserts may be used with V40™ or C-taper femoral heads.

The alphabetical letter at the end of all Trident® catalog numbers identifies compatibility among all Trident® acetabular components. Matching the shell and insert Alpha Codes will ensure proper compatibility.

### Trident® Compatibility Chart

<table>
<thead>
<tr>
<th>Alpha Code</th>
<th>Trident® PSL® HA Shell Size (mm)</th>
<th>Trident® Hemispherical Shell Size (mm)</th>
<th>X3™ 0° and 10° Inserts (mm)</th>
<th>N2/Vac* 0° and 10° Inserts (mm)</th>
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<tbody>
<tr>
<td>A</td>
<td>40</td>
<td>42</td>
<td>22</td>
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<tr>
<td>J</td>
<td>70, 72</td>
<td>72, 74</td>
<td>22, 26, 28, 32, 36</td>
<td>28</td>
</tr>
</tbody>
</table>

N/A = not available

(A) Stryker Orthopaedics Trident Acetabular Inserts made of X3 UHMWPE, 721-00-32E, show a 97% reduction in volumetric wear rate versus the same insert fabricated from N2Vac gamma sterilized UHMWPE, 620-00-32E. The insert tested was 7.5 mm thick with an inner diameter of 32 mm. Testing was conducted under multi-axial hip joint simulation for 3 million cycles using a 32 mm CoCr articulating counterface and calf serum lubricant. X3 UHMWPE Trident acetabular inserts showed a net weight gain due to fluid absorption phenomena but yielded a positive slope and wear rate in linear regression analysis. Volumetric wear rates were 46.39 ± 11.42 mm3/106 cycles for standard polyethylene inserts and 1.35 ± 0.68 mm3/106 cycles for test samples. Testing was performed on un-sterilized X3 UHMWPE Trident acetabular inserts. Although in-vitro hip wear simulation methods have not been shown to quantitatively predict clinical wear performance, the current model has been able to reproduce correct wear resistance rankings for some materials with documented clinical results.[1,2]

(B) X3 UHMWPE meets ASTM F648 for Density as measured per ASTM D1505. X3 UHMWPE exceeds requirements for Tensile Yield Strength, Ultimate Tensile Strength, Elongation and Impact Strength for a Type 3 resin (Tensile strengths and elongation measured per ASTM D638, impact strength per F648, Annex A1). X3 UHMWPE has similar crystalline and lamellar structure as N2Vac gamma sterilized UHMWPE as measured by Small Angle X-ray Scattering (SAXS) and Differential Scanning Calorimetry (DSC) analysis. DSC determined crystallinity was 61.3 ± 0.8% and 61.7 ± 0.6% for N2Vac UHMWPE and X3 UHMWPE, respectively. Lamellar crystal thickness was 23.0 and 23.6 nanometers for N2Vac UHMWPE and X3 UHMWPE, respectively.

(C) X3 UHMWPE shows similar wear particle shape and size as Stryker Orthopaedics Trident Acetabular Inserts made of N2Vac gamma sterilized UHMWPE. Un-sterilized Trident X3 UHMWPE acetabular insert wear debris showed a length of 0.471 ± 0.814 microns, a width of 0.247 ± 0.399 microns and an aspect ratio of 1.99 ± 1.76, while N2Vac UHMWPE polyethylene Trident acetabular insert wear debris showed a length of 0.409 ± 0.533 microns, a width of 0.221 ± 0.356 microns and an aspect ratio of 2.34 ± 3.48. Wear debris was generated from multi-axial hip simulation testing and was isolated following published techniques.[4]

(D) Stryker Orthopaedics Trident Acetabular Inserts made of X3 UHMWPE shows similar wear particle shape and size as Stryker Orthopaedics Trident Acetabular Inserts made of N2Vac gamma sterilized UHMWPE. Un-sterilized Trident X3 UHMWPE acetabular insert wear debris showed a length of 0.471 ± 0.814 microns, a width of 0.247 ± 0.399 microns and an aspect ratio of 1.99 ± 1.76, while N2Vac UHMWPE polyethylene Trident acetabular insert wear debris showed a length of 0.409 ± 0.533 microns, a width of 0.221 ± 0.356 microns and an aspect ratio of 2.34 ± 3.48. Wear debris was generated from multi-axial hip simulation testing and was isolated following published techniques.[4]

References


US Patent 6,475,243

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